

## **CLASS VI GEOMECHANICAL MODELING**

### **INJECTION WELL 357-7R ELK HILLS A1-A2 PROJECT**

#### **Geomechanical Modeling**

##### **Overview**

A finite element geomechanics module, GEOMECH, coupled with Computer Modeling Group's (CMG) equation of state compositional reservoir simulator (GEM), was used to model failure of the Reef Ridge Shale due to increasing pressure in the underlying reservoir by CO<sub>2</sub> injection. A modified Barton-Bandis model can be used to allow CO<sub>2</sub> to escape from the storage reservoir through the cap rock to overburden layers. The location and direction of fractures in a grid block are determined via normal fracture effective stress computed from the geomechanics module.

A generic two-dimensional model was constructed to represent the reservoir, confining layer, and overburden formations. CO<sub>2</sub> is injected through an injector located at the center of the X-Z plane and perforated throughout the reservoir. Increasing pressure in the reservoir is expected to push up and bend the overlying cap rock to create a tensile stress around the high-pressure region. As gas continues to be injected, the normal effective stress in the cap rock is expected to continually decrease. When the cap rock reaches a threshold value, defined as zero in this model, a crack will appear in the cap rock and the Barton-Bandis model will allow CO<sub>2</sub> to leak from the storage reservoir.

##### **Results**

Failure pressures for the four scenarios are given in Table 1. The value for the reduced injection case was extrapolated from the pressure at a stress of about 10 PSI. These results suggest that the Reef Ridge Shale can tolerate a pressure at the base of 7,500 PSI or more without failure.

**Table 1: Geomechanical modeling results for four scenarios.**

<b>GEOMECHANICAL SCENARIO RESULTS</b>	
<b>SCENARIO</b>	<b>FAILURE PRESSURE, psia</b>
BASE CASE	8306
REDUCED YOUNG'S MODULUS	8388
REDUCED INJECTION RATE	8340
THINNER CAP ROCK	7600

### Description

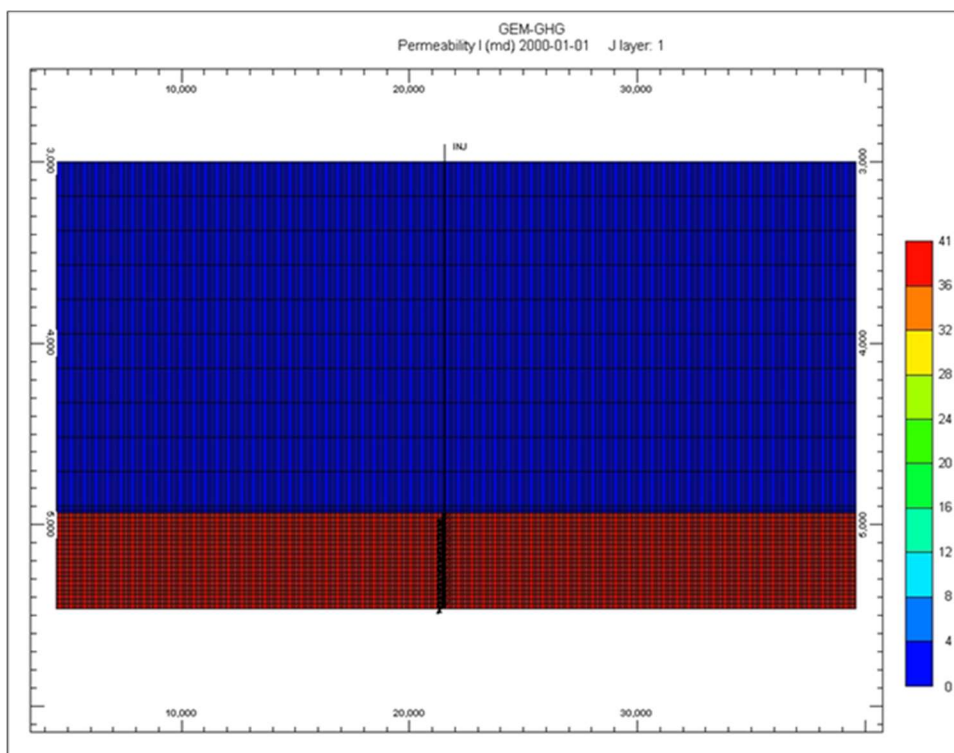
A 2-D cross-section model with 411 grid blocks in the X-direction and 33 grid blocks in the Z-direction was built encompassing a length of 43,100 feet and a thickness of 2,460 feet. This model is shown in Figure 1.

In the base model, the cap rock is 1,935 feet thick with a Young's modulus of 9E05 psi and a Poisson's ratio of 0.23. The reservoir is 525 feet thick with a Young's modulus of 7.25E05 and a Poisson's ratio of 0.25. Horizontal permeability is 1e-07 md in the cap rock and 40.5 md in the reservoir. The vertical to horizontal permeability ratio is 0.25. A constant porosity of 0.25 is used in all zones.

The reservoir is constrained at the bottom but allowed to move at the top and sides. The horizontal direction unconstrained boundary is used to cope with open regions on both the left and right of the modeled portion of the reservoir.

The injector was constrained to inject 30 million cubic feet per day of CO<sub>2</sub> with a maximum injection pressure of 10,000 PSI.

**Figure 1: Geomechanics Model.**



### Scenarios Modeled

Four scenarios were modeled in this study. In the base case, the cap rock has a Young's modulus of 9E05 PSI. To model uncertainty in the cap rock Young's modulus, a second case was run with a value of 8E05 PSI. In the third case, the impact of a thinner cap rock was modeled by assigning a confining layer of 795 feet. In the fourth case, sensitivity to injection rate was studied by reducing the injection rate to 20 million cubic feet per day.

Figure 2 gives the change in the normal fracture effective stress in the bottom cap rock layer and the pressure in the top layer of the reservoir with time for each scenario. The failure pressure is defined as the value at which the effective stress is zero. In the reduced injection rate case the stress stopped decreasing at about 10 PSI, due to CO<sub>2</sub> bleeding into the cap rock despite the very low vertical permeability.

**Figure 2: Normal Fracture Stress and Pressure for Geomechanics Cases.**

